

Erasmus Mundus

Zernike polynomials and beyond

A workshop of the Erasmus Mundus Master course

« Optics in Science and Technology »

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TU Delft

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... and all those interested

- One **introductory** lecture (summary of M1 lectures in the Institut d'Optique master of optical engineering cursus)
- Five **advanced lectures** by guest lecturers
- **Poster** presentations on related issues (teaching, instruments, methods, research results)

Introduction to Zernike circle polynomials for the description of wavefronts and aberrations.

Pierre Chavel

Hervé Sauer,

Gaëlle Lucas-Leclin, Raymond Mercier, Yvan Sortais

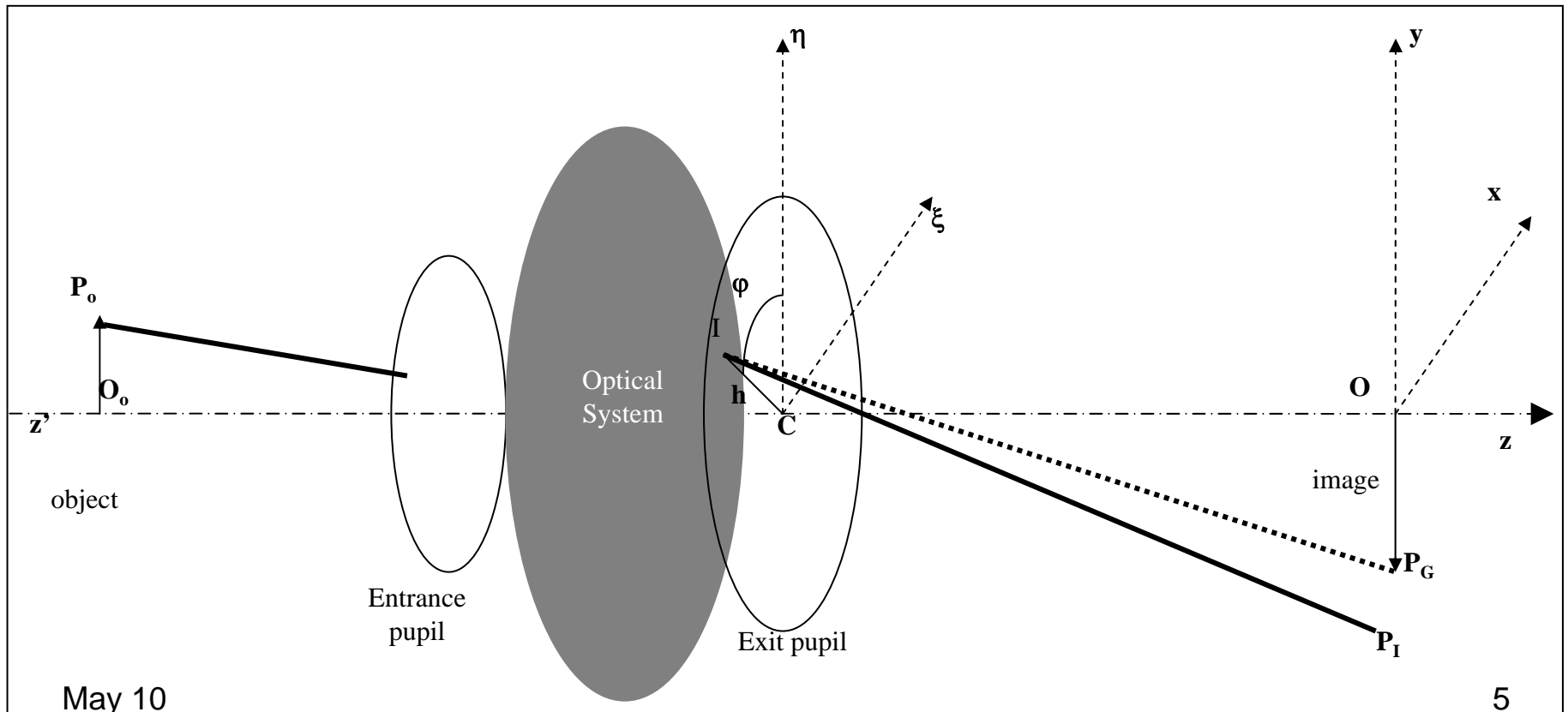
Jean Taboury, Jacques Sabater

Institut d'Optique - *Graduate School*,

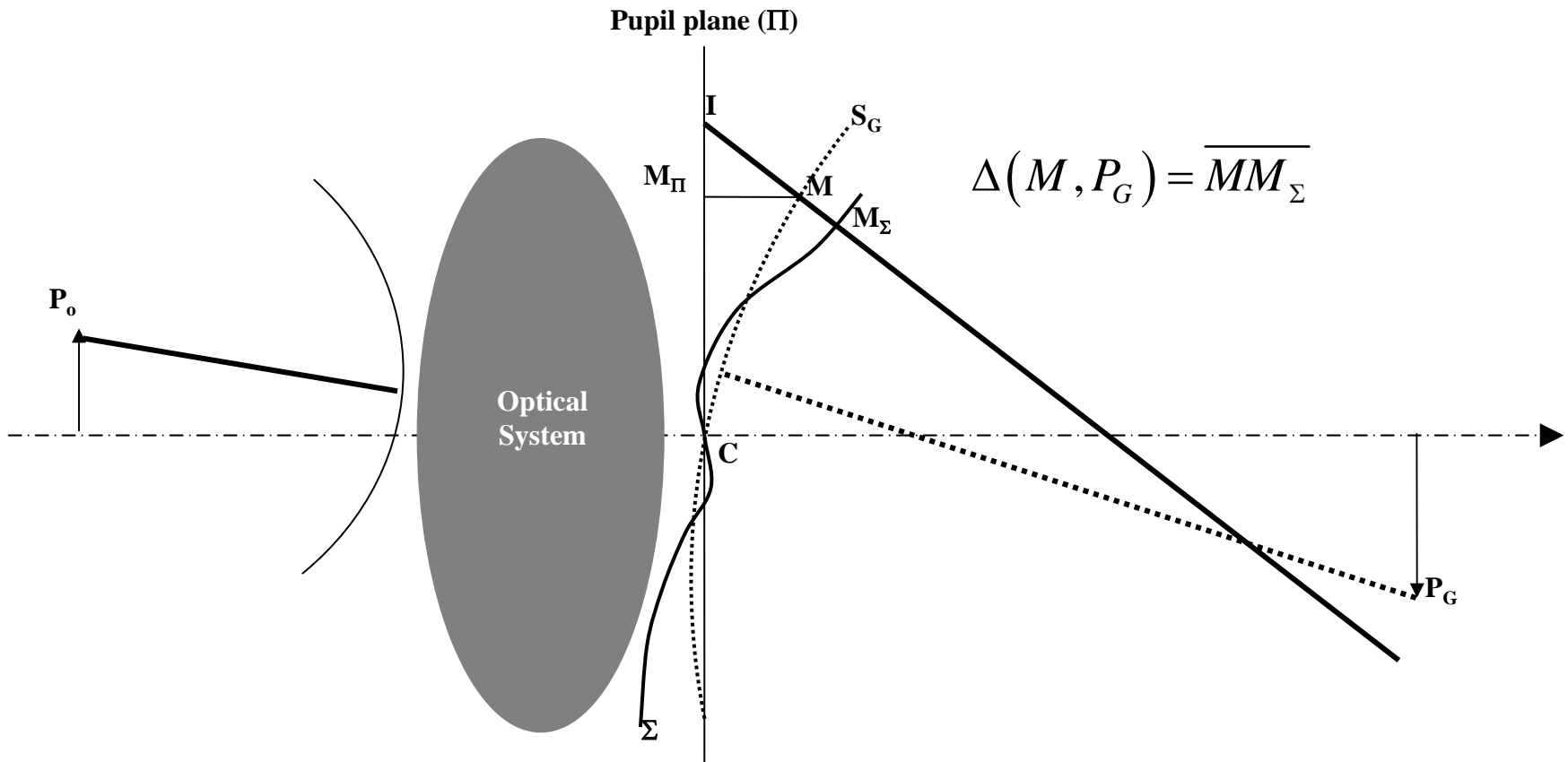
- The need for aberration expansions: system and wavefront parameters
- The Rayleigh-Sommerfeld diffraction integral for aberrated systems
- Aberration classification
 - Seidel
 - Zernike polynomials
 - Orthonormal wavefront expansion
- Applications:
 - 3rd order aberrations
 - Adaptive optics

Consider centered optical system, with identified Gaussian elements.

Arbitrary ray through point I of exit pupil intersects Gaussian image plane at P_I



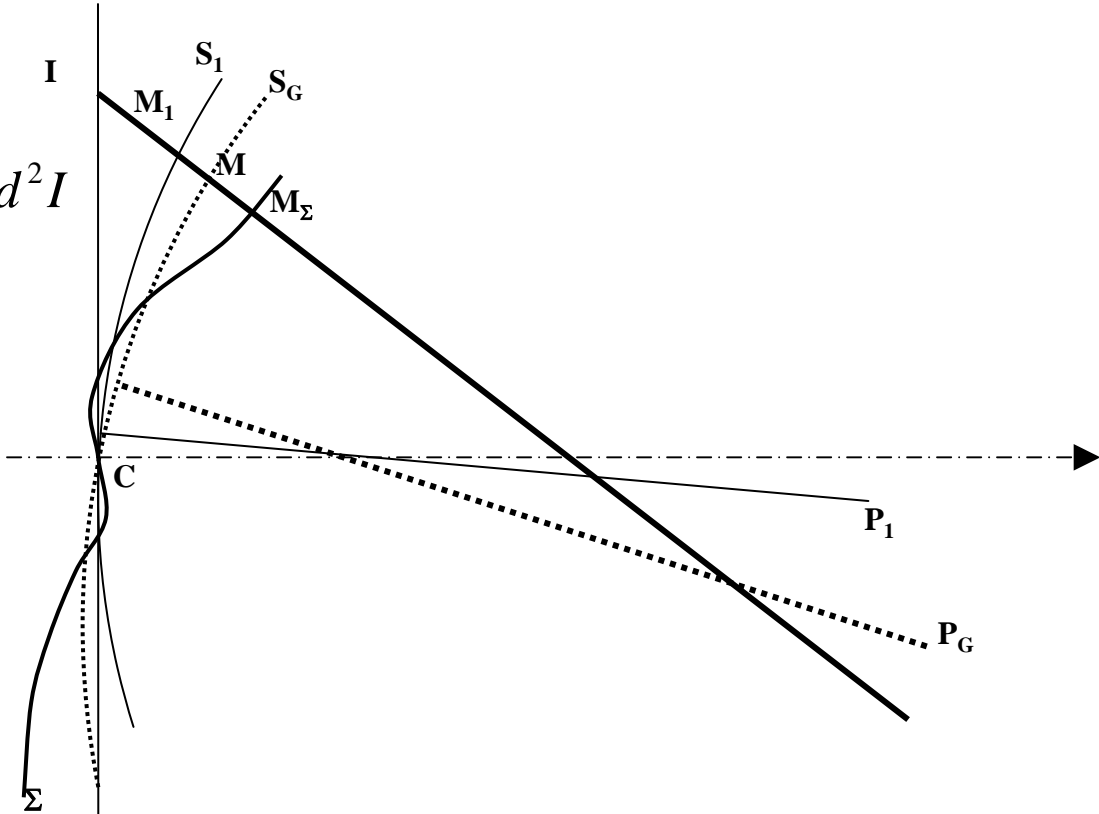
Wavefront departure (path difference)



$$U(P_1) = \frac{-i}{\lambda} \int_S U(I) \frac{\exp(ik IP_1)}{IP_1} \cos \theta d^2 I$$

$$\phi(I) = -k \overline{IM} - k\Delta(M) + \phi_C$$

Pupil plane (Π)



- Assumptions:

- Scalar description valid
- Rayleigh-Sommerfeld integral
- Pupil uniformly illuminated

$$U(P_1) = \frac{-iA \exp(i\phi_C)}{\lambda} \int_{I \in \Pi} \frac{1}{IP_1} \exp \left[\underbrace{-ik\Delta(M) + ikMP}_{\text{Phase } \psi} \right] d^2 I$$

- Under the Fresnel approximation
- and if the denominator is essentially constant,

$$U(P_1) = \frac{-iAe^{i\phi_c + ik(R+\varepsilon)}}{\lambda R}$$

Pupil characteristic function

$$\iint_{\mathbb{R}^2} p_o(\xi, \eta) \exp(-ik\Delta(\xi, \eta)) \exp\left(-ik\varepsilon \frac{\xi^2 + \eta^2}{2R^2}\right) \exp\left(-ik \frac{\xi \delta x_1 + \eta \delta y_1}{R}\right) d\xi d\eta$$

- the resulting amplitude is the Fourier transform of the phase term, focus included (FT of the aberrated pupil function).

- The center of the Airy disk is the absolute maximum of the irradiance that can be obtained in a given plane ($z=R$)

$$E_{MA} = \left(\frac{A\pi a^2}{\lambda R} \right)^2$$

- The image irradiance is an integral of a (space variant!) incoherent « point spread function » weighted by the geometrical image.

- Not rigorously an impulse response in the sense of linear, shift invariant systems.

$$E(\vec{r}) = \int E_{\text{geom}}(\vec{r}_G) \text{IPSF}(\vec{r} - \vec{r}_G, \vec{r}_G) d^2 \vec{r}_G$$

- The « Strehl ratio » is the ratio of the irradiance at a given point to E_{MA} .
- Concurrent definitions exist.

$$R_S = \frac{E_M}{E_{MA}}$$

$$\begin{aligned}
 |U(P_1)|^2 &= \left(\frac{A}{\lambda R}\right)^2 \left| \iint_S e^{i\psi(M)} d^2M \right|^2 = \left(\frac{A\pi a^2}{\lambda R}\right)^2 \left| \frac{\int_0^1 \int_0^{2\pi} \left(1 + i\psi - \frac{\psi^2}{2}\right) u \, du \, d\theta}{\int_0^1 \int_0^{2\pi} u \, du \, d\theta} \right|^2 \\
 &= E_{MA} \left| 1 + i\bar{\psi} - \frac{\overline{\psi^2}}{2} \right|^2 = E_{MA} (1 - \sigma_\psi^2)
 \end{aligned}$$

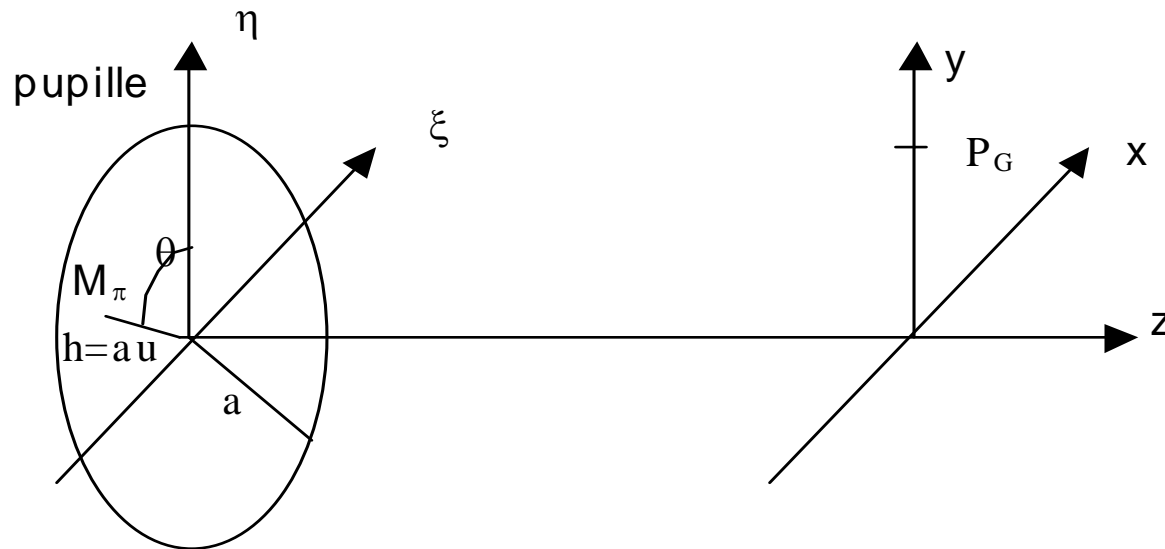
- Nijboer (1943) expansion for small phases: the local irradiance is directly given by the phase variance over the pupil
- Whence the Maréchal criterion (1944):
 - 20% loss for variance $\lambda^2 / 180$

- To get a good feeling of the behaviour
 - of optical systems being designed
 - of wave propagation

an arbitrary phase function is not convenient.

- Here, we consider the important case where a small number of terms of an expansion onto a suitable basis is appropriate.

The Seidel aberrations



$$\Delta(u, y, \theta) = \sum_{(p,q,m) \in \mathcal{N}} A_{pqm} u^{2p+m} y^{2q+m} \cos m\theta$$

- In the most intuitive representation (Seidel 1855), all aberration terms are monomials, not polynomials.
- Aberration order $n=2p+2q+2m-1$

Orders 1 and 3

n	p	q	m	name
1	1	0	0	Defocus
	0	1	0	Vergence from focus
	0	0	1	Tilt
3	2	0	0	Primary spherical
	0	2	0	Primary piston
	0	0	2	Primary astigmatism
	1	1	0	Primary curvature
	1	0	1	Primary coma
	0	1	1	Primary distortion

- Zernike, 1934: given the scalar product

$$(f, g) = \frac{\int_0^1 \int_0^{2\pi} f(u, \theta) g^*(u, \theta) u \, du \, d\theta}{\pi}$$

a complete set of orthogonal polynomials $\mathcal{R}_n^m(u) e^{im\theta}$
of degree n can be defined such that:

$$n \in \mathbb{N}, \quad m \in \mathbb{Z},$$

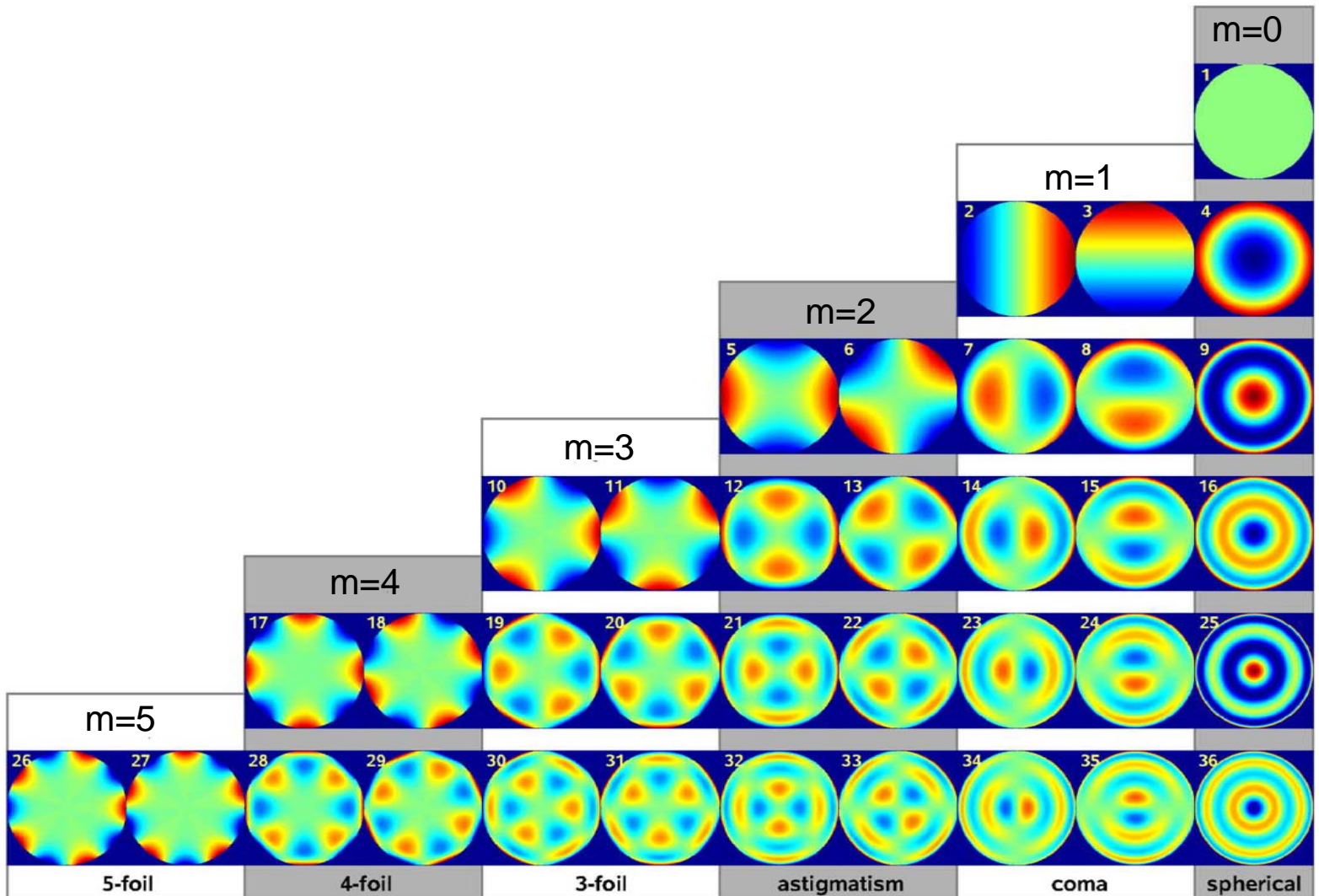
all $n < m$ terms vanish

all terms with $n - m$ odd vanish

$$\mathcal{R}_n^m(0) = 1$$

$\mathcal{R}_0^0(u) = 1$		$\mathcal{R}_2^0(u) = 2u^2 - 1$		$\mathcal{R}_4^0(u) = 6u^4 - 6u^2 + 1$
	$\mathcal{R}_1^1(u) = u$		$\mathcal{R}_3^1(u) = 3u^3 - 2u$	
		$\mathcal{R}_2^2(u) = u^2$		(higher order term)

- All Seidel aberrations up to order 3 are recognized, but associated to other terms



- So, now, what do we call spherical aberration: the Seidel aberration or the Zernike aberration that includes the former as its highest order term?
- V.N. Mahajan: "A Zernike polynomial aberration may also be referred to as a "balanced" aberration. For example, the Zernike primary spherical aberration R^4_0 consists of a classical primary spherical aberration (u^4 term) optimally balanced with defocus (u^2 term) to minimize its variance. It may be called "balanced primary spherical aberrations"."

$$Z_n^m(u, \theta) = \begin{cases} \sqrt{\frac{2(n+1)}{1+\delta_m^0}} \mathcal{R}_n^{|m|}(u) \cos m\theta & \text{for } m \geq 0 \\ -\sqrt{2(n+1)} \mathcal{R}_n^{|m|}(u) \sin m\theta & \text{for } m < 0 \end{cases}$$

$$\Delta(u, y, \theta) = \sum_{(n,q) \in \mathbb{N}^2, m \in \mathbb{Z}} D_{mnq} Z_n^m(u, \theta) y^{2q+m}$$

- Small aberrations: $\frac{E(P_1)}{E_{MA}} = 1 - \frac{4\pi^2}{\lambda^2} \sum_{m,n \neq 0,0} D_{mn}^2$

- There exists also a single index numbering scheme
- Various notations exist. An ISO standard (ISO14999) offers a consensus.

Rayleigh 20% limit

Primary aberration term	Maximum admissible departure	
	At paraxial image	At best focus
sphericity	$0,24 \lambda$	$0,95 \lambda$
coma	$0,20 \lambda$	$0,60 \lambda$
astigmatism	$0,17 \lambda$	$0,17 \lambda$
curvature	$0,25 \lambda$	(Airy)
distorsion	$0,14 \lambda$	(Airy)

- Measure wavefront!
- Include actuators in the setup such that $\delta_p(u, \theta) = V_p \sum_{(m,n) \in \mathbb{N}^2} d_{mnp} Z_n^m(u, \theta)$

- If aberrations can be compensated by the actuators to a good degree, then

$$R_S = 1 - \frac{4\pi}{\lambda^2} \sum_{m,n \neq 0,0} \left(\sum_p V_p d_{mnp} + D'_{mn} \right)^2 Z_n^m(u, \theta)$$

- Minimizing versus V_p :

$$\sum_{m,n} \left(\sum_{p'} V_{p'} d_{mnp'} + D'_{mn} \right) d_{mnp} = 0$$